

Metamaterials and multiphysical couplings [solved with finite elements]

Introduction to finite element modeling for waves and other physical problems with FreeFem++

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v1.3, October 2021

Content

- 1 Principles of the finite element method
- 2 Photonic and phononic crystals
- 3 3D, Vector finite elements (Maxwell equations, elastic waves)
- 4 Multiphysics couplings
- 5 Appendix

Objectives of the lecture

- Basics of the Finite Element Method (FEM)
- Waves (optics, electromagnetism, acoustics) with finite elements
- Show how far you can go with open-source software

Topics:

- 1 Introduction to the language: domain, mesh, variables, weak form, boundary conditions, solving a linear equation (forced response), obtaining eigenvalues and eigenvectors
- 2 2D photonic and sonic crystals (scalar wave equation, periodicity, radiation boundary condition)
- 3 Guided waves in optical planar waveguides and fibers (weak form, light cone)
- 4 Vibrations and modes of mechanical and optical resonators (PML, 3D mesh)
- 5 Acousto-optical coupling in nanophotonics (photoelastic and moving boundary effects, optomechanics)

Partial differential equations (PDE)

A **partial differential equation (PDE)** for the function $u(x, y)$, written as

$$\mathcal{L}u = f$$

over a domain Ω , where \mathcal{L} is a differential operator containing $x, y, u, \frac{\partial u}{\partial x}, \frac{\partial u}{\partial y}$.

Examples:

- **Laplace's** equation: $-\nabla \cdot (\nabla u) = 0$
- **Poisson's** equation: $-\nabla \cdot (\epsilon \nabla \phi) = \rho$
- **Helmholtz's** equation: $-\nabla \cdot (c \nabla u) - k^2 u = 0$

Galerkin's method (*for the dummies*)

Let us consider $\mathcal{L}u = f$ defined over a domain Ω . One can represent (project) u over a base defined by functions w_j , by

$$u(x, y) = \sum_{j=1}^n a_j w_j(x, y)$$

where a_j are coefficients (real or complex).

The PDE is projected over the functions w_i

$$\int_{\Omega} w_i \mathcal{L}u = \int_{\Omega} w_i f, \forall i = 1 \dots n$$

We get a linear equation

$$Aa = f$$

with $A_{ij} = \int_{\Omega} w_i \mathcal{L}w_j$ and $f_i = \int_{\Omega} w_i f$. The formal solution is $a = A^{-1}f$.

Linear equations

Many programs can solve linear equations. General purpose: Matlab, Octave, Python, Julia. Finite element method: Comsol and FreeFem++.

- Matrix inversion:

$$A^{-1}A = I$$

- Linear problem: find x satisfying

$$Ax = f$$

- Eigenvalue problem: find (λ, x) satisfying

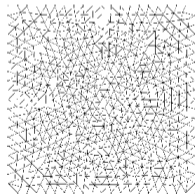
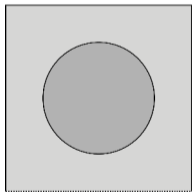
$$Ax = \lambda x$$

- Generalized eigenvalue: find (λ, x) satisfying

$$Ax = \lambda Bx$$

Mesh and sub-domains

- We divide a domain Ω in smaller domains where all coefficients of the differential equation are homogeneous.
- One has to decrease the size of the small domains to improve the result. One has to not decrease it to much to avoid infinite calculation time! Compromising / understanding the problem is the key to find the best mesh.



Most common Boundary Conditions: BC

- 1 A boundary condition which specifies the value of the function itself is a **Dirichlet boundary condition**:

$$u = 0, \text{ or } u = u_0, \text{ on } \sigma$$

- 2 A boundary condition which specifies the value of the normal derivative of the function is a **Neumann boundary condition**:

$$\frac{\partial u}{\partial n} = 0$$

with n the outgoing normal to the boundary σ .

Additional BC (for a given function f):

- 1 Robin: $c_0 u + c_1 \frac{\partial u}{\partial n} = f$
- 2 Mixed: $u = f$ and $c_0 u + c_1 \frac{\partial u}{\partial n} = f \dots$

Finite element space

- Let us consider a domain Ω and its mesh Th . We decide to describe the solution by a finite number of degrees of freedom (*dof*), for example the nodal values u_j^e for the j nodes of the e elements.
- The finite element space Wh is the union of all representable functions by this given choice. Practical important aspect: It is a functional space of finite dimension.
- Representation *inside* a finite element
 $u^e(x, y) = \sum_j N_j^e(x, y) u_j^e$ where $N_j^e(x, y)$ are basis functions.
- For Lagrange elements, P_n , there is continuity of $u(x, y) = \sum_e u^e(x, y)$ between elements. The space derivatives, however, are not continuous!

Weak Form

- Let us assume that we have made a choice on Wh (for a domain Ω and its mesh Th).
- We replace the initial problem $\mathcal{L}u = f$ by an approximation:
Find $u \in Wh$ that solves $\int_{\Omega} w \mathcal{L}u = \int_{\Omega} wf$ for all test functions $w \in Wh$.
- u and w are uniquely determined by their nodal values $U = \{u_j^e\}$ and $W = \{w_j^e\}$.
- There exists a matrix K and a vector B such that

$$W^T K U = W^T B, \forall W$$

- Finally we get a linear equation: $KU = B$

Practical implementation for any FEM software

- 1 Define the domain
- 2 Mesh it
- 3 Choose the type of elements
- 4 Define the BC
- 5 Define the equations (i.e, define their weak form)
- 6 Choose the solver
- 7 Solve!
- 8 Display the results

1D: How does the software solve the problem (Poisson)?

- 1 Projection of the PDE on test functions

$$-\int_0^1 dx \psi(x) \frac{\partial}{\partial x} \left(\epsilon(x) \frac{\partial \phi(x)}{\partial x} \right) = \int_0^1 dx \psi(x) \rho(x)$$

- 2 Integration by parts

$$\int_0^1 dx \frac{\partial \psi}{\partial x} \epsilon \frac{\partial \phi}{\partial x} - \left[\psi \epsilon \frac{\partial \phi}{\partial x} \right]_0^1 = \int_0^1 dx \psi \rho$$

- 3 Application of known BC: $\left[\psi \epsilon \frac{\partial \phi}{\partial x} \right]_0^1$; for example:

- Dirichlet: $\psi(0) = 0$
- Neumann: $\frac{\partial \phi(1)}{\partial x} = 0$

2D: How does the software solve the problem (Poisson)?

- 1 Projection of the PDE on test functions

$$-\int_{\Omega} dr \psi(r) \nabla \cdot (\epsilon(r) \nabla \phi(r)) = \int_{\Omega} dr \psi(r) \rho(r)$$

- 2 Gauss's law

$$\int_{\Omega} dr \nabla \psi \cdot (\epsilon \nabla \phi) - \int_{\sigma} dn \psi \epsilon \frac{\partial \phi(r)}{\partial n} = \int_{\Omega} dr \psi \rho$$

- 3 Application of BC: $\int_{\sigma} \psi \epsilon \frac{\partial \phi(r)}{\partial n}$; for example:

- Dirichlet: $\psi(r) = 0$ over a part of σ
- Neumann: $\epsilon \frac{\partial \phi(r)}{\partial n} = 0$ on the rest of σ

Eigenvalue problem (summary)

- Let us consider a square (real or complex valued) matrix M of dimension n . An eigenvalue problem with eigenvalue λ and eigenvectors u is an equation of the following form $Mu = \lambda u$ ($\sum_{j=1}^n M_{ij}u_j = \lambda u_i$). Eigenvalues are solution of the characteristic polynomial $|M - \lambda I| = 0$.
- There are exactly n eigenvalues and at most n eigenvectors (*a priori* complex). Eigenvectors are nonzero and thus can always be normalized.
- If M is a real symmetric (or Hermitian) matrix, then eigenvalues are real and eigenvectors are orthogonal.
- Generalized eigenvalue problem: $Au = \lambda Bu$

Artificial crystals

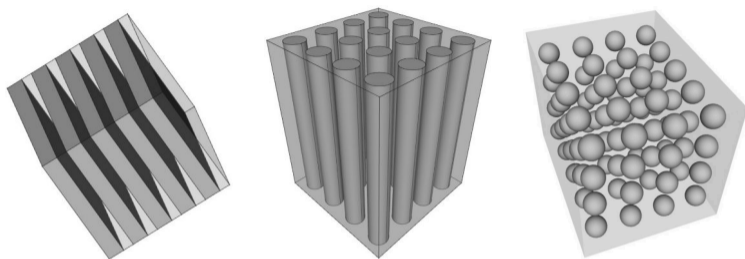


Figure: Artificial crystals for waves with 1D, 2D, or 3D periodicity

- Photonic crystal: matrix and Inclusions are dielectrics
- Sonic crystal: matrix is a fluid (e.g., water or air)
- Phononic crystal: matrix is a solid (e.g., steel, silicon, quartz...)
- Inclusions can be void, solid, or fluid

Acoustics (harmonic)

Acoustic equation for pressure p in the harmonic regime with a source term:

$$-\nabla \cdot (\rho^{-1} \nabla p) - \omega^2 B^{-1} p = f$$

with B the elastic modulus (Pa), ρ the density (kg/m^3), and f a source term ($1/\text{s}^2$).

Example: Loud speaker in a room

- Domain
- BC (pressure, normal acceleration, soft and hard boundary, radiation)?
- Applying a force: Dirichlet or Neumann? Response of the system?
- What is a good mesh for a harmonic problem at a single wavelength λ ?
- Change the finite elements; does the solution change?

TE and TM 2D photonic crystal (harmonic)

Maxwell's equations in the harmonic regime lead to:

- TE (transverse electric field)

$$-\nabla \cdot (\nabla E_z) = \epsilon(\omega/c)^2 E_z$$

- TM (transverse magnetic field)

$$-\nabla \cdot (\epsilon^{-1} \nabla H_z) = (\omega/c)^2 H_z$$

with $\epsilon = n^2$ the relative dielectric permittivity and c the speed of light in a vacuum.

Bloch theorem

Helmholtz equation with periodic coefficients: $-\nabla \cdot (c(\mathbf{r})\nabla u(\mathbf{r})) = \omega^2 u(\mathbf{r})$

Theorem (Bloch)

The eigenmodes of the periodic Helmholtz equation are Bloch waves of the form

$$u(\mathbf{r}) = \exp(-i\mathbf{k} \cdot \mathbf{r})\tilde{u}(\mathbf{r})$$

where $\tilde{u}(\mathbf{r})$ is a periodic function with the same periodicity as the crystal and \mathbf{k} is the Bloch wave vector.

(Classical) band structure: solve for $\omega(k)$

Weak form of the pressure equation, boundary conditions

- Consider all possible test functions $q(t, \mathbf{x})$ belonging to the same finite element space as the pressure and form the scalar products

$$-\int_{\Omega} d\mathbf{x} q \nabla \cdot \left(\frac{1}{\rho} \nabla p \right) + \int_{\Omega} d\mathbf{x} q \frac{1}{B} \frac{\partial^2 p}{\partial t^2} = \int_{\Omega} d\mathbf{x} q f.$$

- Using the divergence theorem, the weak form is

$$\int_{\Omega} d\mathbf{x} \nabla q \cdot \left(\frac{1}{\rho} \nabla p \right) - \int_{\sigma} ds q \left(\frac{1}{\rho} \nabla p \right) \cdot \mathbf{n} + \int_{\Omega} d\mathbf{x} q \frac{1}{B} \frac{\partial^2 p}{\partial t^2} = \int_{\Omega} d\mathbf{x} q f.$$

- External boundary conditions – free: $\left(\frac{1}{\rho} \nabla p \right) \cdot \mathbf{n} = 0$; Dirichlet: $p = p_0$
- Continuity between elements of p and $\left(\frac{1}{\rho} \nabla p \right) \cdot \mathbf{n}$ (normal acceleration)

Example of an internal source and radiation BC

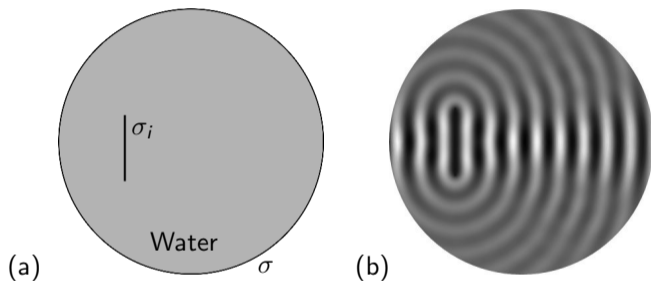


Figure: Internal source and radiation boundary condition. (a) The computational domain is a disk of water inside which a linear source is added by prescribing $p = 1$ Pa along internal boundary σ_i . A radiation boundary condition $\left(\frac{1}{\rho}\nabla p\right) \cdot \mathbf{n} = -i\frac{\omega p}{\rho c}$ is applied at boundary σ . (b) The solution shows the natural diffraction of the acoustic beam radiated from the source. The source dimension is slightly less than 3 wavelengths in water.

FEM for a unit-cell: the band structure of sonic crystals

- Look for Bloch waves in the form $p(\mathbf{r}) = \exp(-i\mathbf{k} \cdot \mathbf{r})\tilde{p}(\mathbf{r})$, and consider $\tilde{p}(\mathbf{r})$ as the unknown field
- In order to obtain the band structure, it is enough to solve the eigenproblem

$$\omega^2 \int_{\Omega} d\mathbf{r} \left(\tilde{q}^* \frac{1}{B} \tilde{p} \right) = \int_{\Omega} d\mathbf{r} \left((\nabla \tilde{q} - i\mathbf{k}\tilde{q})^\dagger \frac{1}{\rho} (\nabla \tilde{p} - i\mathbf{k}\tilde{p}) \right), \forall \tilde{q}$$

- There is no source term and the boundary integral vanishes identically because of the periodic boundary conditions.
- The wave vector \mathbf{k} enters directly the variational formulation, and more precisely the stiffness matrix.

Sonic crystal of cylindrical steel rods in water: band structure

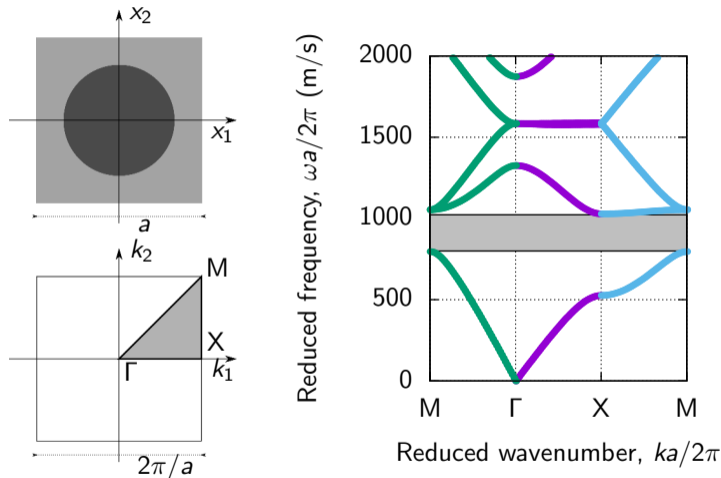
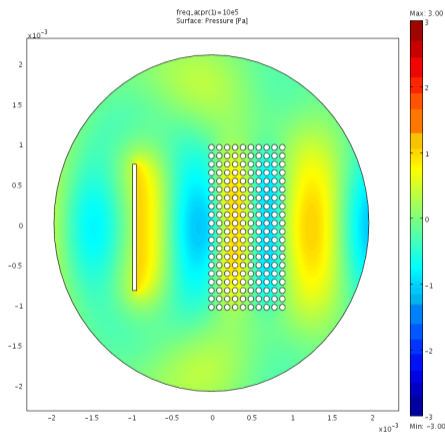


Figure: 2D square-lattice sonic crystal. $d/a = 0.83$

A square-lattice phononic crystal of steel rods in water: transmission



- Pitch: $100 \mu\text{m}$
- Diameter: $70 \mu\text{m}$
- Complete band gap: 8-9 MHz
- Plane source emits 1 Pa

Acoustics (eigenvalue problem) for a special case

Acoustical equation in harmonic regime with an axial wavenumber:

$$-\nabla \cdot (\rho^{-1} \nabla p) + (k_z^2 \rho^{-1} - \omega^2 B^{-1}) p = 0$$

with B the elastic modulus (Pa), ρ the density (kg/m^3), and k_z an axial wave number ($1/\text{m}$).

Example: tubular problem

- Domain
- BC (soft and hard boundary)?
- Find the first 5 eigenvalues?
- change k_z : influence of the length of the tube?

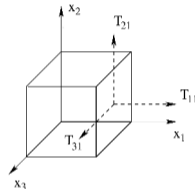
3D elasticity: deformations and strain

- Let us consider a point \mathbf{x} with its coordinates (x_1, x_2, x_3) . $u_i(\mathbf{x} + d\mathbf{x}) = u_i(\mathbf{x}) + \frac{\partial u_i}{\partial x_j} dx_j$ at the first order. $\frac{\partial u_i}{\partial x_j}$ is the displacement gradient.
- One can split this gradient into a symmetric part (S_{ij}) and an antisymmetric part as follows

$$\frac{\partial u_i}{\partial x_j} = S_{ij} + AS_{ij}, \quad S_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \quad \text{and} \quad AS_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} - \frac{\partial u_j}{\partial x_i} \right)$$
- The symmetric part gives the deformation or **strain** and the antisymmetric part the local rotations.
- The dilation is given by $S = S_{11} + S_{22} + S_{33} = \nabla \cdot \mathbf{u}$.
- Terms S_{11} , S_{22} and S_{33} are longitudinal strains and $S_{ij}, i \neq j$, are transverse strains.

3D Elasticity: Stresses

- 3 independent constraints can be applied on a surface: a traction-compression and two shear constraints.



- On the face of the cube normal to x_1 , the force per unit of surface is $T_{11} + T_{21} + T_{31}$. T_{ij} is a rank-two symmetric tensor called the **stress tensor**. For a surface denoted by its normal n , the traction is given by the vector $T_{ij}n_j$.
- Dynamical (or Navier) equation (with f_i the internal forces):
$$\frac{\partial T_{ij}}{\partial x_j} + f_i = \rho \frac{\partial^2 u_i}{\partial t^2}$$

3D elasticity: Hooke's law

- For small deformations Hooke's law can be expressed as :

$$T_{ij} = c_{ijkl} S_{kl}$$

i/e. the stress is proportional to the strain.

- c_{ijkl} is a 4th order tensor, called elasticity tensor. It has *a priori* $3^4 = 81$ components. Assuming symmetry of T_{ij} and S_{kl} implies that $c_{jikl} = c_{ijkl}$ et $c_{ijkl} = c_{ijlk}$. reducing it to 36 independent components.
- Adding the major symmetry $c_{ijkl} = c_{klij}$ only 21 components are left.

3D elasticity: Notations

$$(11) \rightarrow 1; (22) \rightarrow 2; (33) \rightarrow 3$$

$$(23) = (32) \rightarrow 4; (13) = (31) \rightarrow 5; (12) = (21) \rightarrow 6$$

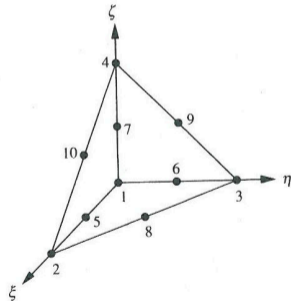
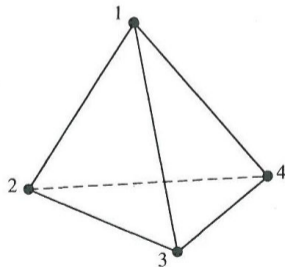
$$T_I = T_{ij}; c_{IJ} = c_{ijkl}; T_I = c_{IJ} S_J$$

$$S_1 = S_{11}; S_2 = S_{22}; S_3 = S_{33}; S_4 = 2S_{23}; S_5 = 2S_{13}; S_6 = 2S_{12}$$

Matériaux	Classe	Rigidités (10^{10} N/m ²)					ρ (10^3 kg/m ³)
cub. ou isotrope		c_{11}	c_{12}	c_{44}			
AsGa	$\bar{4}3m$	11.88	5.38	2.83			5.307
SiO ₂	isotrope	7.85	1.61	3.12			2.203
Si	$m\bar{3}m$	16.56	6.39	7.95			2.329
hexagonal		c_{11}	c_{12}	c_{13}	c_{33}	c_{44}	
PZT-4	trans. iso.	13.9	7.8	7.4	11.5	2.6	7.5
ZnO	$6mm$	21.0	12.1	10.5	21.1	4.2	5.676
trigonal		c_{11}	c_{12}	c_{13}	c_{33}	c_{44}	c_{14}
Al ₂ O ₃	$\bar{3}m$	49.7	16.3	11.1	49.8	14.7	-2.3
LiNbO ₃	$3m$	20.3	5.3	7.5	24.5	6.0	0.9
quartz α (SiO ₂)	32	8.7	0.7	1.2	10.7	5.8	-1.8

3D Mesh

- In 2D one can mesh the domain using triangles.
- In 3D one may use tetrahedrons.



Vector finite elements

- Let's consider a vector field (u_1, u_2, u_3) .
- A domain Ω and its mesh Th . One describes the solution by a finite number of DOF
- A vector finite space of elements Wh is a finite set of representable functions by this choice.
- Representation *in* a finite element
 $u_i^e(x, y) = \sum_j N_j^e(x, y) u_{ij}^e$ where $N_j^e(x, y)$ are basis functions as in the scalar case.
- For Lagrange elements, P_n , the continuity $u_i(x, y) = \sum_e u_i^e(x, y)$ between elements is preserved.

Weak form for 3D elasticity (1)

- 1 Elastodynamic equation:

$$-\nabla T + \rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \mathbf{f}$$

- 2 Projection on the vector test functions \mathbf{v} :

$$-\int_{\Omega} \mathbf{v} \cdot \nabla T + \int_{\Omega} \mathbf{v} \cdot \rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \int_{\Omega} \mathbf{v} \cdot \mathbf{f}$$

- 3 Divergence theorem:

$$\int_{\Omega} \nabla_{\mathbf{v}} T - \int_{\sigma} \mathbf{v} \cdot \mathbf{T}_n + \int_{\Omega} \mathbf{v} \cdot \rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \int_{\Omega} \mathbf{v} \cdot \mathbf{f}$$

Weak form for 3D elasticity (2)

- 1 Hooke's law: $T_I = c_{IJ}S_J$ with $S = \nabla u$

$$\int_{\Omega} S(v)_I c_{IJ} S(u)_J - \int_{\sigma} v \cdot T_n + \int_{\Omega} v \cdot \rho \frac{\partial^2 u}{\partial t^2} = \int_{\Omega} v \cdot f$$

- 2 BC: $\int_{\sigma} v \cdot T_n$ is known:

- Dirichlet: $v = 0$ on a part of σ (clamped)
- Neumann: $T_n = 0$ on the remaining part σ (stress free)

- 3 monochromatic case (or harmonic excitation)

$$\int_{\Omega} S(v)_I c_{IJ} S(u)_J - \int_{\sigma} v \cdot T_n - \omega^2 \int_{\Omega} v \cdot \rho u = \int_{\Omega} v \cdot f$$

Example: Bending of a beam under gravity

- Clamped silicon beam.
- bending by gravity in the static case.
- Visualization of the deformation.

Eigenmode of a beam

- Clamped on two sides.
- neglect gravity
- Find the eigenmodes
- influence of the BC?

Multiphysics: coupling of different physical problems

- Many physical models are coupled and many phenomena or even moduli depend on one another
 - Electro-optics, magneto-optics
 - Piezoelectricity
- Equations are linked by constitutive relation
- *One must consider a vector finite element space containing all unknowns of the problem.*

Example: piezoelectricity

- Direct piezoelectric effect: an electric polarization is induced by a deformation.
- Inverse piezoelectric effect: an applied electric field induces a deformation of the crystal lattice.
- The piezoelectric effect only appears in non centro-symmetric crystals.
- Coupled equations (e_{kij} : piezoelectric tensor)

$$T_{ij} = c_{ijkl}S_{kl} - e_{kij}E_k; D_i = e_{ikl}S_{kl} + \epsilon_{ij}E_j$$

- Electric field derives from a potential : $E_i = -\frac{\partial\phi}{\partial x_i}$
- In contracted form:

$$T_I = c_{IJ}S_J - e_{kl}\phi_{,k}; D_i = e_{iJ}S_J + \epsilon_{ij}\phi_{,j}$$

Indirect coupling of physical models

- Many different situations lead to coupled multiphysics models
 - A system can perform a distant action on another system, for instance a force...
 - If a physical quantity induces a deformation of the system, then the geometry and the mesh must change, and thus the solution can change even there was no direct coupling in the equation...
- There is no simple rule to decide how to solve the problem: a coupling model has to be improvised!

Some useful integral theorems

V a volume, S a surface enclosing the volume. \oint stands for an integral over a **closed** surface or contour.

- Gradient theorem

$$\int_V dV \nabla f = \oint_S \mathbf{n} f dS$$

- Gauss theorem (or divergence theorem)

$$\int_V dV \nabla \cdot \mathbf{f} = \oint_S dS \mathbf{n} \cdot \mathbf{f}$$

- Rotational theorem

$$\int_V dV \nabla \times \mathbf{f} = \oint_S dS \mathbf{n} \times \mathbf{f}$$