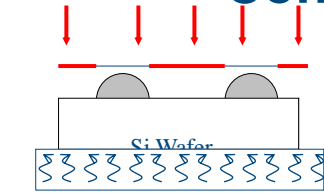
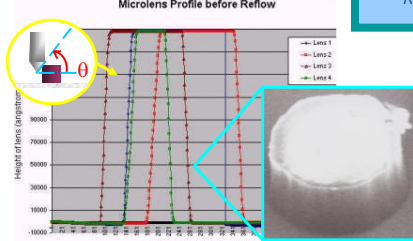


Convex lens - fabrication



Photoresist Clariant AZ9260

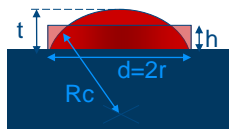


Process	Speed (mm)	Temp (°C)	UV Irr. (mW/cm ²)	Duration (s)
Spin-coat	1000	/	/	60
Pre-bake	/	100	/	300
Exposure	/	/	10	200
Development	/	/	/	600
Reflow	/	115	/	900



Chollet F., Low C. H., Lee S. K., Yang C., "Fabrication of concave and convex micro-optical elements with polymer for free-space micro-optical bench", Int. J. of Computation. Eng. Sci., vol. 4, n. 3 (2003) : 443-446

Convex lens - model



$$768\pi VR_c^3 - 12\pi^2 d^4 R_c^2 -$$

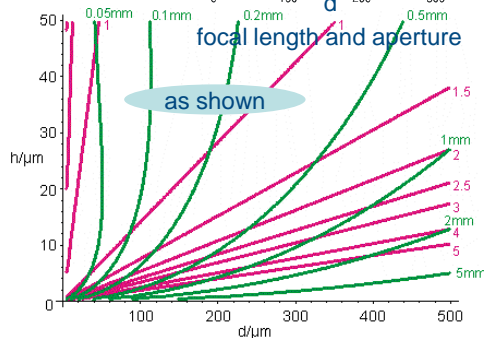
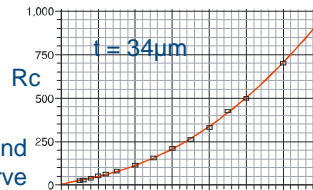
$$576V^2 - \pi^2 d^6 = 0$$

$V = h \pi (d/2)^2$
 $f = R_c * (n-1)$ - lens maker's equation
 $\# = f/d$ - relative aperture

■ The model assumes that:

- the diameter d does not change on reflow
- the reflow creates a spherical profile

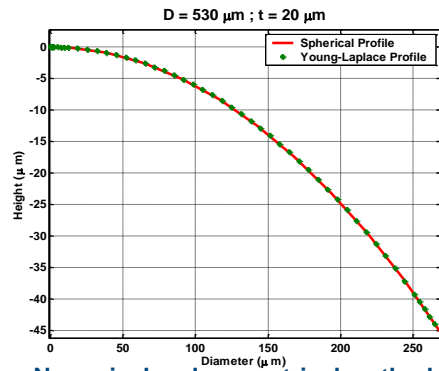
Experimental and theoretical curve



Convex lens - model

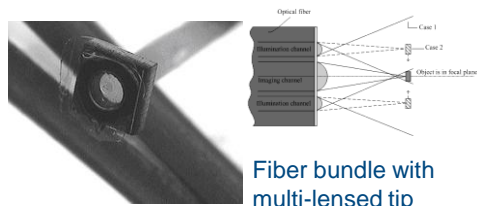
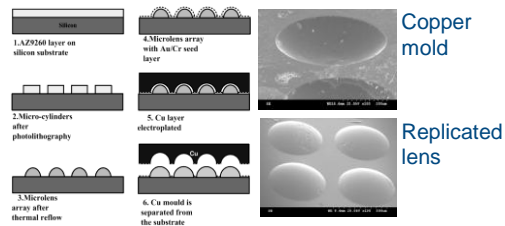
- The profile can also be obtained as a solution of Young-Laplace equation
- The equation can be solved numerically with the ability to see the effect of other parameter like gravity (g), density of molten polymer (ρ_L), surface tension of molten polymer (γ)...
- Even this solution is not complete as it does not take into account the dynamic of melting and solidification

$$\frac{d^2y/dx^2}{\sqrt{(1+(dy/dx)^2)^3}} + \frac{dy/dx}{x\sqrt{1+(dy/dx)^2}} = \frac{(\rho_L - \rho_V)gy}{\gamma} + \frac{2}{R_0}$$



Microlens - application

- Production of copper lens insert for molding of fiber coupling array
- Imaging/illumination fiber for endoscopic application



Ashraf M., Chollet F., Murukeshan VM., Yang C., "Fabrication of polymer-based reflowed microlenses on optical fibre with control of focal length using differential coating technique", Sadhana, doi:10.1007/s12046-009-0038-5, Vol. 34, No. 4, (2009) : 607-613